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Small signal stability analysis of stand-alone microgrid with composite load



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Abstract

Microgrid concept provides suitable context for installing distributed generation resources and providing reliability and power quality for loads. During grid connected mode of microgrid, all stability issues are getting handled by main grid due to its sufficient inertia. But when islanding occurs, microgrid faces stability-related problems. This paper presents the state space model of isolated microgrid along with load dynamics. This paper investigates the effect of static load, induction motor type of dynamic load and composite load on the stability of the island microgrid. The paper also studies the effect of damping and inertia on the stability of the microgrid. The performance of the test system is evaluated using MATLAB simulation software. The present studies show that during the planning of the microgrid, effect of types of loads and load changes should be considered for stable operation of the system.

Keywords: Island, Microgrid, Eigenvalues, Small signal stability, Load modelling, Composite load

Introduction

The integration of distributed generation with the main grid is called microgrid. Microgrid is the combination of small sources, like renewable energy sources, network and the loads. The inverter is main interfacing part of microgrid, and it can be considered as a source. Microgrid enhances the overall power generation and reliability of the power system. Due to use of power electronics devices, microgrid has a lot of issues related to power quality, stability and neutral current. Therefore, it is necessary to consider the effect of source location, location of load, type of load and load parameter before the installation of microgrid. The loads can be classified as static load, dynamic load and composite load. Static loads are the algebraic function of voltage and frequency, and it is composed of constant impedance characteristics, constant current characteristics and constant power characteristics. Generally, static loads do not affect on the stability of the system because it considers only present values of the system data. One main disadvantage of the static model is that in addition to ignoring the dynamics of the dynamic load; it does not take into consideration the effect of the load inertia constant [1]. The dynamic loads affect the stability of the microgrid because it considers the present as well as historical data during performance. The load modelling of dynamic load like induction machine is to be carried out accurately for voltage stability analysis [2].



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Composite load modelling consists of combination of static load and dynamic load. The superiority has increased due to aggregated dynamic load representation in both small and large disturbance studies. Composite load modelling is important for accurate modelling because the dynamic model can only express the dynamic response of load model [3]. When the influence of distributed generation is not negligible, the induction motor load model cannot effectively describe the actual load characteristic [4]. While planning of microgrid, it is most important to consider the composite loads. During the planning of microgrid, it is most important to study impacts of load dynamics on the stability [5].

Considerable attention has been given in the literature to consider the effect of constant power load (CPL) on the small signal stability of the island microgrid [6-8]. However, the analysis of an islanded microgrid system based on a state space model of the CPL does not essentially guarantee the stability of the system. Ariyasinghe et al. [6] suggested a state space model of a constant power load model of islanded microgrid to investigate the small signal stability. In their study, authors do not present the effect of loading and damping. The study also limited up to three bus system with 2 generators and one load. In [7], the small signal stability framework is carried out for studying the islanded microgrid system for constant load under the different uncertainty condition. The simulation was carried on the 9 bus DC microgrid system. Authors were not considered the effect of dynamic load conditions. So, this model would not perfect for stability analysis of islanded microgrid. Amelian et al. [9] have discussed the comprehensive effect of dynamic load and static load on microgrid stability. But this paper has not discussed the effect of damping and inertia on stability. In [10], dynamic load model is considered for stability analysis of microgrid. The author has considered medium voltage microgrid for analysis. Guzman et al. [11] presented the dynamics of inverter-based islanded microgrid. The bifurcation theory was used to present the oscillation and load margin of the composite load. Kallamadi et al. [12] have discussed small signal stability analysis of microgrid for static and dynamic load, but authors do not discuss about the composite load. Pogaku et al. discussed [13] the effect of inverter parameters on the stability of microgrid. A sensitivity analysis was presented to analyse the stability. Hossain et al. [8] discussed stability microgrid for constant power loads only with pole zero location for the different cases. The effect of PID controller is also presented in the paper, and simulation model was developed on the MATLAB software. In [14] state space model of isolated microgrid with wind energy source and two types of loads, heating and induction machines and their effect on stability have been discussed.

The microgrid stability is getting disturbed while the transition of AC microgrid from grid connected mode to the stand-alone mode [19]. The effect of energy storage system on the stand-alone microgrid is presented in [20]. To fulfil the power generation and load demand in the stand-alone microgrid system, energy storage system and energy management system can be integrated [20, 21]. As microgrid is working in stand-alone mode, the energy storage system can be used for fulfiling the load demand. The effect of constant power loads and constant current loads on the DC microgrid and their effect on stability have been witnessed in [22]. A Lyapunov stability theory was presented to analyse the dynamic stability, which revealed that the eigenvalues of constant power loads affect more as compared to the constant current loads. In [23], the effect

of constant power loads, droop gain and line impedance on the small signal stability of dc microgrid is investigated. The analysis reveals that as the droop gain is increased the system becomes more unstable.

When microgrid connects to main grid, the load dynamics does not affect the stability because of its sufficient inertia (Because main grid has more inertia as compared to microgrid). After islanding, microgrid faces stability-related problems because of its low inertia. Hence, in this paper stability analysis of islanded microgrid is studied in detail.

The main contributions of the present research paper are

- 1. Detailed state space model of the microgrid with composite load for stability analysis.
- Discussed the effect of eigenvalues of static load, induction motor load and composite load on the stability of the system.
- 3. Discussed the effect of change in composite load on stability analysis.
- 4. Discussed the effect of damping and inertia on the small signal stability of the islanded microgrid with composite load.

In most of the literatures, only static loads or dynamic loads are considered for stability analysis of microgrid. In the present research paper, small signal stability analysis of microgrid with composite load is investigated and the results of composite load are compared with the static and dynamic load. The eigenvalue technique is used for stability analysis of microgrid [15]. The synchronous reference frame (SRF) method is considered for modelling of microgrid system. The study shows that the microgrid stability depends on the types of loads. Composite loads are more participating in stability analysis of microgrid system. Increasing the damping and inertia value within a certain limit improves the stability of microgrid.

Methods

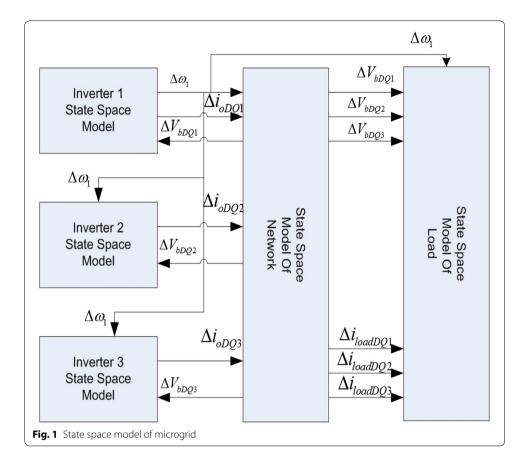
The state space model of microgrid used for the stability analysis is shown in Fig. 1. In Fig. 1, there are three inverters, which are considered as sources (because all the sources in microgrid are integrated with the system using inverters). The output frequency of inverter one is taken as a reference.

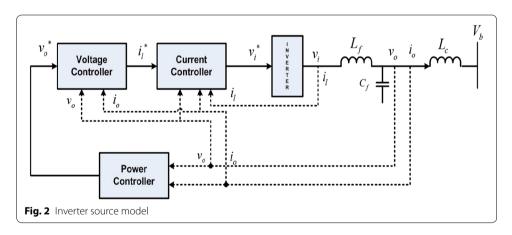
Mathematical modelling of microgrid

In this section, mathematical modelling of the source, load and network are presented. Inverter source model, composite load model and network model are presented in detail as below.

Source model

The photovoltaic cell, diesel generator, wind turbine are the main sources of microgrid. But power is getting injected into the grid through inverters; therefore, it is called as the source of the system. The detailed mathematical model is given in this section [13, 16]. The complete inverter source model of the system is given in Fig. 2; it consists of power controller, voltage controller and current controller. These controllers are required for interconnection of the inerter with point of common coupling (PCC).





Equation 1 describes the dynamics of inverter in the form of the state space model. The state variables affect the stability of inverter and finally stability of microgrid.

$$[\Delta x_{\rm inv}] = A_{\rm inv}[\Delta x_{\rm inv}] + B_{\rm inv}[\Delta \nu_{\rm bDQ}] + B_{\omega_{\rm com}}[\Delta \omega_{\rm com}]$$
(1)

$$\begin{bmatrix} \Delta \omega \\ \Delta i_{\text{oDQ}} \end{bmatrix} = \begin{bmatrix} C_{\text{inv}\omega} \\ C_{\text{inv}c} \end{bmatrix} [\Delta x_{\text{inv}}]$$
(2)

where Δx is the dynamic state variable vector, Δx_{inv} is a state variable vector, A_{inv} is the state matrix of inverters, B_{inv} , $B_{\omega co}$, $C_{inv\omega}$ and C_{invc} are the input matrix of inverters, $[\Delta v_{bDQ}]$ is a bus voltage vector, $[\Delta \omega_{com}]$ is the reference frequency vector, and ΔI_{oDQ} is an output current matrix in the DQ reference frame.

Load model

Loads are energy consuming part of the system. The loads may be static, dynamic or composite load.

RL load

The equations given below describe the state of the RL load with the changes in frequency, resistance and inductance of the load.

$$A_{\text{load1}} = \begin{bmatrix} -\frac{R_{\text{load1}}}{L_{\text{load1}}} & \omega\\ -\omega & -\frac{R_{\text{load1}}}{L_{\text{load1}}} \end{bmatrix}$$
(3)

$$A_{\text{load2}} = \begin{bmatrix} -\frac{R_{\text{load2}}}{L_{\text{load2}}} & \omega\\ -\omega & -\frac{R_{\text{load2}}}{L_{\text{load2}}} \end{bmatrix}$$
(4)

$$B_{1\text{load1}} = \begin{bmatrix} \frac{1}{L_{\text{load1}}} & 0\\ 0 & \frac{1}{L_{\text{load1}}} \end{bmatrix}, \quad B_{2\text{load1}} = \begin{bmatrix} \Delta i_{\text{loadQ1}}\\ -\Delta i_{\text{loadD1}} \end{bmatrix},$$

$$B_{1\text{load2}} = \begin{bmatrix} \frac{1}{L_{\text{load2}}} & 0\\ 0 & \frac{1}{L_{\text{load2}}} \end{bmatrix}, \quad B_{2\text{load2}} = \begin{bmatrix} \Delta i_{\text{loadQ2}}\\ -\Delta i_{\text{loadD2}} \end{bmatrix}$$
(5)

where A_{load1} , A_{load2} are the state matrix of the load, $B_{1\text{load1}}$, $B_{1\text{load2}}$, $B_{2\text{load1}}$ and $B_{2\text{load2}}$ are the input matrix of the load, R_{load} is the resistance of RL load, L_{load} is the inductance of RL load and ω is the frequency of RL load.

Constant impedance, current and power load

The constant impedance, current and power model are also known as ZIP model or static load. In this model, the impedance, current and the power remain constant, but the actual voltage keeps changing. In ZIP model, active power (P) and reactive power (Q) are expressed in terms of exponent a and b, respectively. The detail ZIP model is presented in [17].

Equations 6 and 7 describe the active and reactive power changes for static load, while Eq. 8 gives the relation between constant of the active and reactive power

$$\frac{P}{P_0} = K_{pz} \left(\frac{V}{V_0}\right)^2 + K_{pi} \left(\frac{V}{V_0}\right) + K_{pp} + K_{p1} \left(\frac{V}{V_0}\right)^{n_{pv1}} (1 + n_{pf1}(f - f_0)) + K_{p2} \left(\frac{V}{V_0}\right)^{n_{pv2}} (1 + n_{pf2}(f - f_0))$$
(6)

$$\frac{Q}{Q_0} = K_{qz} \left(\frac{V}{V_0}\right)^2 + K_{qi} \left(\frac{V}{V_0}\right) + K_{qp} + K_{q1} \left(\frac{V}{V_0}\right)^{n_{qv1}}
\left(1 + n_{qf1}(f - f_0)\right) + K_{q2} \left(\frac{V}{V_0}\right)^{n_{qv2}} \left(1 + n_{qf2}(f - f_0)\right)$$
(7)

$$K_{pz} = 1 - \left(K_{pi} + K_{pp} + K_{p1} + K_{p2}\right) \tag{8}$$

where *P* and *Q* are the active power and reactive power, respectively, Subscript '0' identifies the value of respective variable at the initial operating condition, K_{pz} , K_{qz} are the constant impedance component for active power and reactive power, respectively, K_{pi} , K_{qi} are the constant current component for active power and reactive power, respectively, $K_p n_{pv}$, $K_q n_{qv}$ are the constant power component for active power and reactive power, respectively.

Equations 9 and 10 describe the d-axis and q-axis reference frame current, respectively, where Eq. 11 represents the change in d-axis reference frame current with respect to the parameter of load. These equations give the interrelationship between the current, voltage and power for the static load.

$$I_d = P\left(\frac{V_d}{V^2}\right) + Q\left(\frac{V_q}{V^2}\right) \tag{9}$$

$$I_q = P\left(\frac{V_q}{V^2}\right) - Q\left(\frac{V_d}{V^2}\right) \tag{10}$$

$$\Delta I_{d} = \left[\frac{V_{d0}^{2}}{V_{0}^{4}} P_{0}a + \frac{V_{q0}V_{d0}}{V_{0}^{4}} Q_{0}b + \frac{P_{0}}{V_{0}^{2}} + \left(-\frac{2}{V_{0}^{4}}\right) \left(P_{0}V_{d0}^{2} + Q_{0}V_{d0}V_{q0}\right) \right] \Delta V_{d} + \left[\frac{V_{q0}^{2}}{V_{0}^{4}} Q_{0}b + \frac{V_{d0}V_{q0}}{V_{0}^{4}} P_{0}a + \frac{Q_{0}}{V_{0}^{2}} + \left(-\frac{2}{V_{0}^{4}}\right) \left(P_{0}V_{q0}V_{d0} + Q_{0}V_{q0}^{2}\right) \right] \Delta V_{q}$$
(11)
+
$$\left[\frac{P_{0}V_{d0}}{V_{0}^{2}}c + \frac{Q_{0}V_{q0}}{V_{0}^{2}}d \right] \Delta f$$

The dynamics of d-axis reference framed load with the variable voltages, current, active power and reactive power is represented by Eqs. 12, 13 and 14 as given below

$$Y_1 = \frac{1}{V_0^2} \left[\frac{V_{d0}^2}{V_0^2} P_o a + \frac{V_{q0} V_{d0}}{V_0^2} Q_0 b + P_0 + \left(P_0 V_{d0}^2 + Q_0 V_{d0} V_{q0} \right) \left(-\frac{2}{V_0^4} \right) \right]$$
(12)

$$Y_{2} = \frac{1}{V_{0}^{2}} \left[\frac{V_{q0}^{2}}{V_{0}^{2}} Q_{o}b + \frac{V_{q0}V_{d0}}{V_{0}^{2}} P_{0}a + Q_{0} + \left(P_{0}V_{q0}V_{d0} + Q_{0}V_{q0}^{2} \right) \left(-\frac{2}{V_{0}^{4}} \right) \right]$$
(13)

$$Y_{f1} = \frac{1}{V_0^2} \left[P_0 V_{d0} c + Q_0 V_{q0} d \right]$$
(14)

where a and c represent the coefficients of active power which describes the constant power, constant current and constant impedance coefficients for active power, b and drepresent the coefficients of reactive power which describes the constant power, constant current and constant impedance coefficients for reactive power.

These constants in terms of static characteristics of load are expressed by Eqs. 15–18 as presented given below,

$$a = 2K_{pz} + K_{pi} + K_{p1}n_{pv1} + K_{p2}n_{pv2}$$
⁽¹⁵⁾

$$b = 2K_{qz} + K_{qi} + K_{q1}n_{qv1} + K_{q2}n_{qv2}$$
(16)

$$c = K_{p1}n_{pf1} + K_{p2}n_{pf2} \tag{17}$$

$$d = K_{q1}n_{qf1} + K_{q2}n_{qf2} \tag{18}$$

where K_{pp} , K_{qp} , K_{p1} , K_{p2} , K_{q1} , K_{q2} , n_{pv1} , n_{pv2} , n_{qv1} , n_{qv2} are the static characteristics of the load.

Equation 19 represents the change in q-axis reference frame current with respect to the parameter of load. The dynamics of d-axis reference framed load with the variables such as voltages, current, active power and reactive power is represented by Eqs. 20, 21 and 22.

$$\Delta I_{q} = \left[\frac{V_{q0}^{2}}{V_{0}^{4}} P_{0}a - \frac{V_{d0}V_{q0}}{V_{0}^{4}} Q_{0}b + \frac{P_{0}}{V_{0}^{2}} + \left(-\frac{2}{V_{0}^{4}} \right) \left(P_{0}V_{q0}^{2} - Q_{0}V_{q0}V_{d0} \right) \right] \Delta V_{q} + \left[\frac{V_{d0}V_{q0}}{V_{0}^{4}} P_{0}a - \frac{V_{q0}^{2}}{V_{0}^{4}} Q_{0}b - \frac{Q_{0}}{V_{0}^{2}} + \left(-\frac{2}{V_{0}^{4}} \right) \left(P_{0}V_{q0}V_{d0} + Q_{0}V_{d0}^{2} \right) \right] \Delta V_{d} \quad (19) + \left[\frac{P_{0}V_{q0}}{V_{0}^{2}}c - \frac{Q_{0}V_{d0}}{V_{0}^{2}}d \right] \Delta f$$

$$Y_{3} = \frac{1}{V_{0}^{2}} \left[\frac{V_{q0}V_{d0}}{V_{0}^{2}} P_{0}a - \frac{V_{d0}^{2}}{V_{0}^{2}} Q_{o}b + Q_{0} + \left(P_{0}V_{d0}V_{q0} - Q_{0}V_{d0}^{2} \right) \left(-\frac{2}{V_{0}^{4}} \right) \right]$$
(20)

$$Y_4 = \frac{1}{V_0^2} \left[\frac{V_{q0}^2}{V_0^2} P_0 a - \frac{V_{q0} V_{d0}}{V_0^2} Q_0 b + P_0 + \left(P_0 V_{q0}^2 - Q_0 V_{q0} V_{d0} \right) \left(-\frac{2}{V_0^4} \right) \right]$$
(21)

$$Y_{f2} = \frac{1}{V_0^2} \left[P_0 V_{q0} c - Q_0 V_{d0} d \right].$$
(22)

Dynamic load

In most of the system's static load are considered, but load changes with respect to changes in system parameters hence dynamic load model study is important. The equations given below describe the modelling of induction motor, whose dynamics changes to the variables of induction motor such as current, flux, frequency, etc.

$$\frac{1}{\omega_{\rm b}}\frac{\mathrm{d}\varphi_{ds}}{\mathrm{d}t} = -R_{\rm s}i_{ds} + \frac{\omega}{\omega_{\rm b}}\varphi_{qs} + \nu_{ds} \tag{23}$$

$$\frac{1}{\omega_{\rm b}}\frac{\mathrm{d}\varphi_{dr}}{\mathrm{d}t} = -R_{\rm r}i_{dr} + \frac{\omega - \omega_{\rm r}}{\omega_{\rm b}}\varphi_{ds} + \nu_{dr} \tag{24}$$

$$\frac{1}{\omega_{\rm b}}\frac{\mathrm{d}\varphi_{qs}}{\mathrm{d}t} = -R_{\rm s}i_{qs} - \frac{\omega}{\omega_{\rm b}}\varphi_{ds} + \nu_{qs} \tag{25}$$

$$\frac{1}{\omega_{\rm b}}\frac{\mathrm{d}\varphi_{qr}}{\mathrm{d}t} = -R_{\rm r}i_{qr} + \frac{\omega - \omega_{\rm r}}{\omega_{\rm b}}\varphi_{qr} + v_{qr} \tag{26}$$

$$\varphi_{ds} = (X_{\rm s} + X_{\rm m})i_{ds} + X_{\rm m}i_{dr} \tag{27}$$

$$\varphi_{dr} = X_{\rm m} i_{ds} + (X_{\rm r} + X_{\rm m}) i_{dr} \tag{28}$$

$$\varphi_{qs} = (X_{\rm s} + X_{\rm m})i_{qs} + X_{\rm m}i_{qr} \tag{29}$$

$$\varphi_{qr} = X_{\rm m}i_{qs} + (X_{\rm r} + X_{\rm m})i_{qr} \tag{30}$$

$$T_{\rm e} = \varphi_{\rm qr} i_{\rm dr} - \varphi_{\rm dr} i_{\rm qr} \tag{31}$$

$$T_{\rm m} = T_0 \left(\frac{\omega_{\rm r}}{\omega_{\rm b}}\right)^{\beta} \tag{32}$$

$$X_{\rm IM} = A_{\rm IM} X_{\rm IM} + B_{\rm 1IM} \Delta V + B_{\rm 2IM} \Delta \omega \tag{33}$$

$$y = C_{\rm IM} X_{\rm IM} \tag{34}$$

Here, state variable X_{IM} , ΔV and y are represented by the following equation

$$X_{\rm IM} = \begin{bmatrix} \Delta i_{\rm ds} \\ \Delta i_{\rm dr} \\ \Delta i_{\rm qs} \\ \Delta i_{\rm qr} \\ \Delta \omega_{\rm r} \end{bmatrix}, \quad \Delta V = \begin{bmatrix} \Delta V_{\rm ds} \\ \Delta V_{\rm qs} \end{bmatrix}, \quad y = \begin{bmatrix} \Delta i_{\rm ds} \\ \Delta i_{\rm qs} \end{bmatrix}$$
(35)

where $T_{\rm e}$ is the electrical torque, $T_{\rm m}$ is mechanical torque, $\varphi_{\rm ds}$, $\varphi_{\rm dr}$, $\varphi_{\rm qr}$, φ_{dr} are the flux linkages for stator and rotor, i_{dr} , i_{ds} , $i_{\rm qs}$, $i_{\rm qr}$ are the currents through stator and rotor of induction motor, $X_{\rm IM}$ are the state variables of induction motor, $\omega_{\rm b}$ is the base angular speed, $\Delta \omega_{\rm r}$ is the rotor frequency, $A_{\rm IM}$ is the state matrix of induction motor, $B_{1\rm IM}$, $B_{2\rm IM}$, $C_{\rm IM}$ are the inputs for induction motor, $R_{\rm s}$ and $R_{\rm r}$ are stator and rotor resistances, respectively, $X_{\rm s}$ is stator leakage reactance and $X_{\rm m}$ is the magnetizing reactance and ΔV is voltages of the induction motor with DQ reference frame.

Network model

The source model and load model are interlinked by using network model. For stability analysis of network model, RL network is considered [16]. The equations given below describe the dynamics of the network with line resistance, inductance and the bus voltages.

$$\frac{di_{\text{lineD1}}}{dt} = -\frac{r_{\text{line1}}}{L_{\text{line1}}}i_{\text{lineD1}} + \omega i_{\text{lineQ1}} + \frac{1}{L_{\text{line1}}}V_{bD1} - \frac{1}{i_{\text{line1}}}V_{bD2}$$
(36)

$$\frac{di_{\text{lineQ1}}}{dt} = -\frac{r_{\text{line1}}}{L_{\text{line1}}}i_{\text{lineQ1}} + \omega i_{\text{lineD1}} + \frac{1}{L_{\text{line1}}}V_{\text{bQ1}} - \frac{1}{i_{\text{line1}}}V_{\text{bQ2}}$$
(37)

$$\frac{di_{\text{lineD2}}}{dt} = -\frac{r_{\text{line2}}}{L_{\text{line2}}}i_{\text{lineD2}} + \omega i_{\text{lineQ2}} + \frac{1}{L_{\text{line2}}}V_{\text{bD2}} - \frac{1}{i_{\text{line1}}}V_{\text{bD3}}$$
(38)

$$\frac{\mathrm{d}i_{\mathrm{lineQ2}}}{\mathrm{d}t} = -\frac{r_{\mathrm{line2}}}{L_{\mathrm{line2}}}i_{\mathrm{lineQ2}} + \omega i_{\mathrm{lineD2}} + \frac{1}{L_{\mathrm{line2}}}V_{\mathrm{bQ2}} - \frac{1}{i_{\mathrm{line1}}}V_{\mathrm{bQ3}}$$
(39)

Equations. 40 and 41 give the state space model for network 1 and network 2, respectively.

$$\begin{bmatrix} \Delta i_{\text{lineD1}} \\ \Delta i_{\text{lineQ1}} \end{bmatrix} = A_{\text{NET1}} \begin{bmatrix} \Delta i_{\text{lineD1}} \\ \Delta i_{\text{lineQ1}} \end{bmatrix} + B_{1\text{NET1}} \Delta V_{\text{b}} + B_{2\text{NET1}} [\Delta \omega], \tag{40}$$

$$\begin{bmatrix} \Delta i_{\text{lineD2}} \\ \Delta i_{\text{lineQ2}} \end{bmatrix} = A_{\text{NET2}} \begin{bmatrix} \Delta i_{\text{lineD2}} \\ \Delta i_{\text{lineQ2}} \end{bmatrix} + B_{1\text{NET2}} \Delta V_{\text{b}} + B_{2\text{NET2}} [\Delta \omega]$$
(41)

Here, variable $\Delta V_{\rm b}$ are represented by the following equation

$$\Delta V_{\rm b} = \begin{bmatrix} V_{\rm bD1} \\ V_{\rm bQ1} \\ V_{\rm bD2} \\ V_{\rm bQ2} \\ V_{\rm bD3} \\ V_{\rm bQ3} \end{bmatrix}$$
(42)

where A_{NET} is state matrix of the network, ω is the frequency, r_{line} is the line resistance, L_{line} is the line inductance, $B_{1\text{NET1}}$, $B_{1\text{NET2}}$, $B_{2\text{NET1}}$, $B_{2\text{NET2}}$ are the input matrices for network, Δi represents the state variables in the form of current and ΔV_b are the components of bus voltages.

System modelling

Models of inverter, network and load are transferred to a common reference frame. Complete islanded microgrid is obtained by combining all state space models of inverter, network, and load is formulated by Eq. 43

$$A_{\rm mg} = \begin{bmatrix} A_{\rm INV} + B_{\rm INV} R_{\rm N} M_{\rm INV} C_{\rm INVC} & B_{\rm INV} R_{\rm N} M_{\rm NET} & B_{\rm INV} R_{\rm N} M_{\rm LOAD} \\ B_{\rm INET} R_{\rm N} M_{\rm INV} C_{\rm INVC} + B_{\rm 2NET} C_{\rm INVC} & A_{\rm NET} + B_{\rm 1NET} R_{\rm N} M_{\rm NET} & B_{\rm 1NET} R_{\rm N} M_{LOAD} \\ B_{\rm 1LOAD} R_{\rm N} M_{\rm INV} C_{\rm INVC} + B_{\rm 2LOAD} C_{\rm INVC} & B_{\rm 1LOAD} R_{\rm N} M_{\rm NET} & A_{\rm LOAD} + B_{\rm 1LOAD} R_{\rm N} M_{\rm LOAD} \end{bmatrix}$$

$$(43)$$

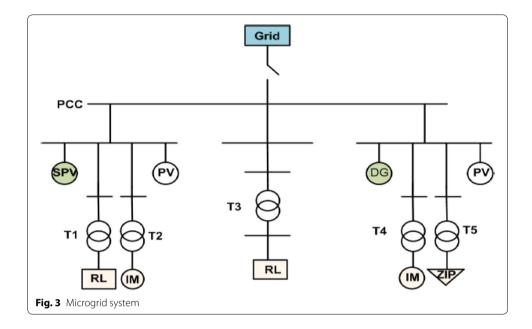


Table 1 Inverter parameters

Parameter	Parameter name	Value	Parameter	Parameter name	Value
Fs	Switching frequency	8 kHz	Mp	Active droop gain	9.4 × 10 ⁻⁵
L _f	Inductance of filter	1.35 mH	N _q	Reactive droop gain	1.3×10^{-3}
C _f	Capacitance of filter	50 × 10 ⁻⁶ F	K _{pv}	Proportional gain of PI (volt- age controller block)	0.05
R _f	Resistance of filter	0.1 Ohm	K _{iv}	integral gain of PI (voltage controller block)	390
L _c	Coupling inductance	0.35 mH	K _{pc}	Proportional gain of PI (cur- rent controller block)	10.5
r _{Lc}	Resistance of coupling inductor	0.03 Ω	K _{ic}	integral gain of PI (current controller block)	16×10^{3}
W _c	Cut off frequency	31.41 rad/s	F	Feed forward gain	0.75

Parameter	Value	Parameter	Parameter
V _{od}	[380.8, 381.8, 380.4] V	V _{oq}	[0,0,0] V
I _{od}	[11.4, 11.4, 11.4] A	I _{oq}	[-0.4, -1.45, 1.25] A
l _{Id}	[11.4, 11.4, 11.4] A	I _{lq}	[-5.5, -7.3, -4.6] A
V _{bd}	[379.5, 380.5, 379] V	V_{bq}	[−6, −6, −5] V
Wo	314 (rad/s)	D_0	[0.1, 9e—3, — 0.0113] degree
I _{line1d}	[-3.8] A	l _{line1g}	[0.4] A
l _{line2d}	[7.6] A	l _{line2q}	[— 1.3] A

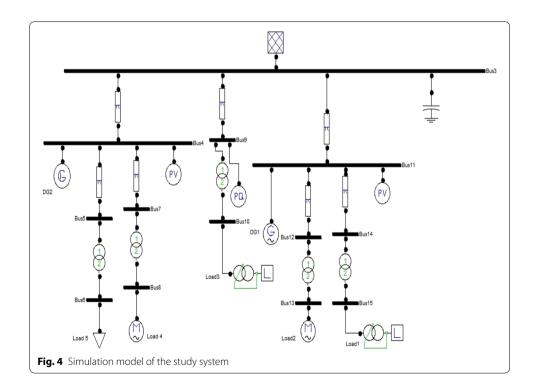
Table 2 Initial conditions of system

Parameter	Values (Ω)	Parameters	Values
R _{Line1}	0.23	R _{Load1}	25 Ohm
X _{Line1}	0.1	L _{Load2}	38.54 mH
R _{Line2}	0.35	R _{Load1}	20 Ohm
X _{Line2}	0.58	L _{Load2}	30.83 mH

Table 3 Network and load parameters

Table 4 Parameters of microgrid

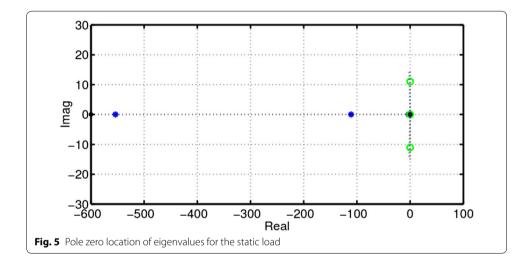
Sr. no.	Parameters	Ratings
1	Utility source	100 MVA, 69 kV
2	$V_{\rm base}$	13.8 kV
3	S _{base}	10 MVA
4	DG1	5 MVA
5	DG2	2.5 MVA
6	Load 1	0.8 MW, 0.47 MVAr
7	Load 2	1.5 MW, 1 MVAr
8	Load 3	3.2 MW, 1.9 MVAr
9	Load 4	0.9 MW, 0.6 MVAr
10	Load 5	0.9 MW



	nposite
15	
15	
1	
19	
1	
4	
40	
	1

 Table 5 Eigenvalues comparison for ZIP load, RL load, dynamic load and composite load

 model



where $A_{\rm mg}$ is the state matrix of microgrid, $A_{\rm INV}$ is the state matrix of inverter, $R_{\rm N}$ is neutral resistance, $A_{\rm NET}$ is the state matrix of network, $A_{\rm LOAD}$ is state matrix of load, $M_{\rm NET}$ matrix gives connecting lines into the network and $M_{\rm LOAD}$ matrix gives connecting lines into the load.

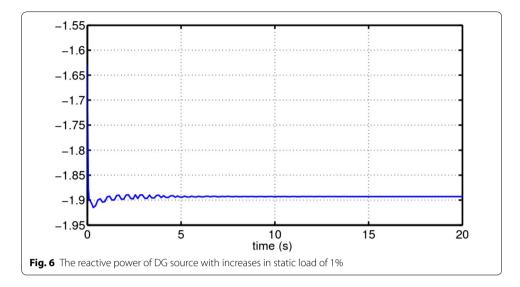
It would not be reliable to consider only static load or only dynamic load while considering small signal stability. The microgrid or any distributed generation is a combination of static loads and dynamic loads. For the above reason in this paper, we analyse the stability of islanded microgrid with composite load. To study the effect of composite load on stability, following equation is formulated,

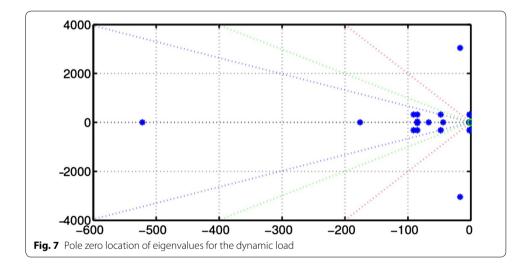
$$A_{\text{Load}} = A_{\text{RL}} + A_{\text{ZIP}} + A_{\text{Dynamic}} \tag{44}$$

The effect of damping and inertia on stability is also taken into the account during the study.

Results

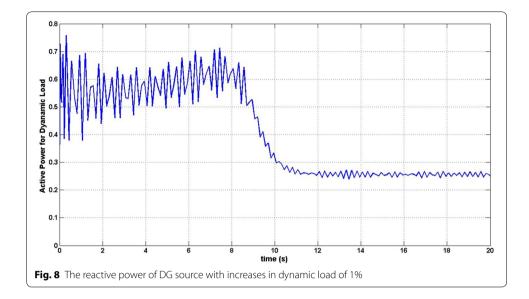
The test system as shown in Fig. 3 is taken from [18] with base kV of 13.8 kV and base MVA of 10 MVA.

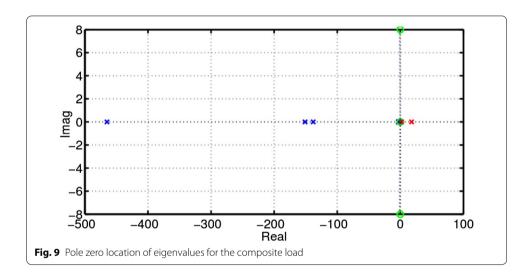




For experimental verification of the system, 10 kVA inverter is considered. The parameter value of the inverter is listed in Table 1. In Table 1, the gain parameters $M_{\rm p}$, $N_{\rm q}$, $K_{\rm pv}$, $K_{\rm iv}$, $K_{\rm pc}$, $K_{\rm ic}$ and F are dimensionless. The initial value of the parameter of the considered system is presented in Table 2. The parameter for the load and network is given in Table 3, while parameter of the considered microgrid is displayed in Table 4.

From Table 1, it is evident that the switching frequency of the proposed network is considered as 8 kHz. The higher value of the switching frequency gives wide control limit. The coupling inductance (L_c) is used to provide coupling impedance between inverter output and interconnection bus, for better voltage regulation. The current feed forward gain (F) is used to provide low output impedance. This model composed three micro-sources (DG1, DG2 and DG3), 5 loads (two induction motors, two RL and one

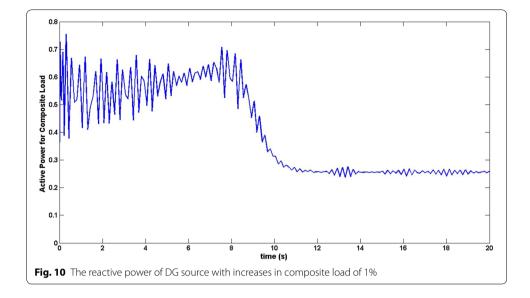




ZIP). The simulation model of the study system is simulated in the Power System Analysis Toolbox of the MATLAB environment as shown in Fig. 4.

In the present research, we investigated the effect of load, damping and inertia of the microgrid system. The eigenvalues of the three types of the load namely static (RL Load), dynamic (Induction motor) and composite load appear in Table 5.

From Table 5, it is visible that the numbers of the eigenvalues of the dynamic load are more as compared to static load, i.e. the nature of load affects the number of eigenvalues. The natures of the load also affect the other parameter of system such as active power, reactive power and speed. These parameters are discussed in subsequent sections.



Eigenvalues	Normal load	Increase in load by 10%
Negative	32	26
Positive	1	2
Real	34	14
Complex	0	10
Zero	1	6
Total	68	58

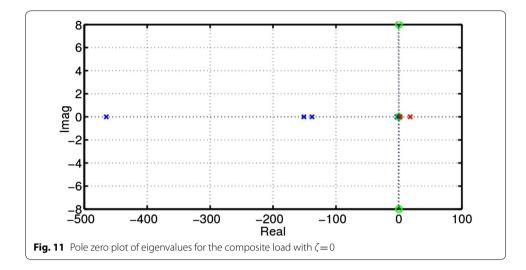
Table 7 Effect of damping on micro-grid with composite load

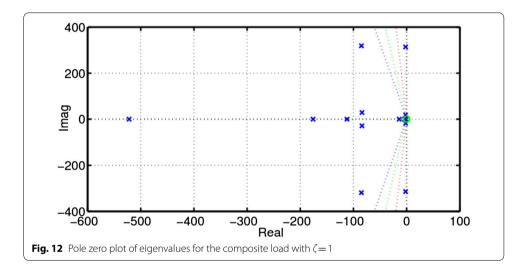
Eigenvalues	$\zeta = 0$	ζ=1	ζ=10	ζ=100
Negative	15	15	19	19
Positive	2	0	0	0
Real	19	19	19	21
Complex	1	1	1	0
Zero	4	6	2	2
Total	41	41	41	41

Effect of load

System with static load

With static load, numbers of the eigenvalues are very few. In the present case, the numbers of negative eigenvalues are 5 as detected in Table 5. The pole zero representation of eigenvalues of the static load is shown in Fig. 5. Figure 5 shows that all the eigenvalues are located on the left hand side plane. It indicates that the parameter of static load not much affecting the stability. The reactive power of DG source with increases in static



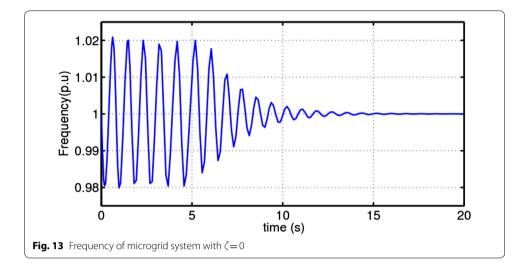


load of 1% is exhibited in Fig. 6. It is observed from Fig. 6 that after 5 s reactive power consumption of DG source is almost constant.

System with dynamic load

With a dynamic load like induction motor, the numbers of the eigenvalues are more because it considers both past as well as present data. Figure 7 gives the pole zero location of eigenvalues for the dynamic load. From Fig. 7, it is clear that the parameter of dynamic load much affected the stability. Hence, during the planning of microgrid study the effect of induction motor is important.

The reactive power of DG source with increases in dynamic load of 1% is given in Fig. 8. From Fig. 8, it is clear that initially the speed of the motor is increasing so system is not more stable and it is oscillating up to 10 s. After 10 s, induction motor



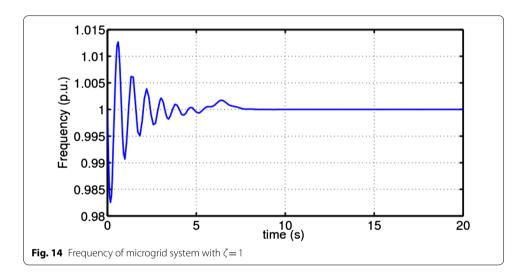


Table 8 Inertia affecting on system operation

Eigenvalues	H=3	H=5.8	H=7
Negative	13	15	16
Positive	2	1	0
Real	19	19	11
Complex	1	2	5
Zero	5	24	5
Total	21	21	21

speed is constant, so it is acting like static load. The reactive power consumption of the dynamic load is more as compared to the RL loads.

System with composite load

With composite load, the numbers of eigenvalues are 40 as presented in Table 5. It is seen from Table 5 that one of the eigenvalues of the composite load is located on the right hand side plane, which make system towards instability and too much unhealthy for microgrid performance. The pole zeroes location of eigenvalues of the composite load are shown in Fig. 9. The eigenvalue with red colour in Fig. 9 shows the positive eigenvalue that moves the system towards instability. The consumption of reactive power at DG source with composite load is shown in Fig. 10. It is observed from Fig. 10 that reactive power consumption of composite load is increased and it is constant after 10 s.

The effect of increases of load by 10%, on the eigenvalues and stability, is demonstrated in Table 6. It is visible from Table 6 that as when the load is increased by 10%, the numbers of positive eigenvalues are increased from 1 to 2 as compared to normal load. The increases in positive eigenvalues make the system more unstable. It indicates that if the composite load increases, microgrid system is moving towards instability.

Effect of damping

The performance of microgrid system with different value of damping is presented in Table 7. From Table 7, it is clear that when $\zeta = 0$, two poles of the system are lying on the right hand side plane, while when $\zeta > 1$, none of the poles lie on the right hand side plane.

The pole zeroes plots of the eigenvalues for the composite load with $\zeta = 0$ and $\zeta = 1$ are presented in Figs. 11 and 12, respectively. From Fig. 11, it is visible that when damping of the system is zero, one of the eigenvalue is located on the right hand side plane and makes the system unstable. From Fig. 12, it is investigated that when the damping of the system is one, all the eigenvalue of microgrid system are lying on the left hand side of the plane and system is more stable. From the above discussion, it is clear that as the damping of the system is increased from $\zeta = 0$ to $\zeta = 1$, stability of the system is increasing.

The frequency plot of the microgrid system with $\zeta = 0$ and $\zeta = 1$ is presented in Figs. 13 and 14, respectively. It is seen from Fig. 13 that system stables after 15 s. Also from Fig. 14, it is clear that system frequency is stable before 10 s. From the above discussion, it is observed that the damping of the system is increased, frequency oscillation is decreased.

Effect of inertia (H)

As we know that the main power system has rotating part, so it has more inertia, but in the present study, we consider microgrid with static devices so there is less inertia. The inertia can be increased by using switching FACT devices in the system. In this present work, we consider three different values of inertia as 3, 5.8 and 7 as shown in Table 8. Table 8 shows that the stability of microgrid system is increased if inertia is increased from 3 to 7.

Conclusion

A complete state space model of microgrid with inverter dynamics, network dynamics and load dynamics is presented in this paper. All these three parts of microgrid are individually modelled and transferred to a common reference frame. During the planning of microgrid, it is necessary to consider the effects of the load parameters on the stability of microgrid hence here in this paper complete load modelling is carried out. The effect of dynamic and composite load parameters on the stability of the microgrid is considered and presented in the paper. The active and reactive power consumption of the microgrid system is different for the RL load, dynamic load and composite load. From the results, it is apparent that dynamic load and the composite load affect system stability more as compared to RL Load. Damping and inertia also affect the stability of the system. From the outcome, it is apparent that the stability of the microgrid system is increased when damping and inertia are increasing. The paper also presented the detail analysis of pole zero location for all the considered parameter. Hence, small signal stability analysis is most important for microgrid system for reliable operation of the power system. Compensation techniques can also be used to investigate its effect on stability and to locate compensator at proper place optimization techniques can be used. The hardware experimental setup will be developed for the simulation model of the test system for further study and validation of the results.

Abbreviations

SRF: synchronous reference frame; PCC: point of common coupling; CPL: constant power load; ZIP: constant impedance, current and power load; P: active power; Q: reactive power.

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Authors' contributions

AB conducted literature review, interpretation of the data and provide the resources for the paper, RA and CDD conducted mathematical modeling, implementation of the simulation model in the MATLAB environment and wrote the paper. All authors read and approved the final manuscript.

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All authors confirm that all relevant data are included in the article in the section 4 from Table 1 to Table 4.

Competing interests

Not applicable.

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